



**زتونة المجالات**

## Vector Calculus

### Convert Between [ POINTS ]

- Cylindrical to Cartesian

$$x = \rho \cos \phi \quad ; \quad y = \rho \sin \phi \quad ; \quad z = z$$

- Cartesian to Cylindrical

$$\rho = \sqrt{x^2 + y^2} \quad ; \quad \phi = \tan^{-1} \left( \frac{y}{x} \right) \quad ; \quad z = z$$

- Spherical to Cartesian

$$x = r \sin \theta \cos \phi \quad ; \quad y = r \sin \theta \sin \phi \quad ; \quad z = r \cos \theta$$

- Cartesian to Spherical

$$r = \sqrt{x^2 + y^2 + z^2} \quad ; \quad \theta = \cos^{-1} \left( \frac{z}{r} \right) \quad ; \quad \phi = \tan^{-1} \left( \frac{y}{x} \right)$$

### Convert Between [ Vectors ]

#### Cartesian-Cylindrical

	$\mathbf{a}_\rho$	$\mathbf{a}_\phi$	$\mathbf{a}_z$
$\mathbf{a}_x \cdot$	$\cos \phi$	$-\sin \phi$	0
$\mathbf{a}_y \cdot$	$\sin \phi$	$\cos \phi$	0
$\mathbf{a}_z \cdot$	0	0	1

#### Cartesian - Spherical

	$\mathbf{a}_r$	$\mathbf{a}_\theta$	$\mathbf{a}_\phi$
$\mathbf{a}_x \cdot$	$\sin \theta \cos \phi$	$\cos \theta \cos \phi$	$-\sin \phi$
$\mathbf{a}_y \cdot$	$\sin \theta \sin \phi$	$\cos \theta \sin \phi$	$\cos \phi$
$\mathbf{a}_z \cdot$	$\cos \theta$	$-\sin \theta$	0

Scalar triple product	Vector triple product
$\bar{\mathbf{A}} \cdot (\bar{\mathbf{B}} \times \bar{\mathbf{C}}) = \begin{vmatrix} x_A & y_A & z_A \\ x_B & y_B & z_B \\ x_C & y_C & z_C \end{vmatrix}$ <p>تمثل مساحة متوازي المستطيلات لو بتساوي صفر اذن هم على مستوى واحد</p> $\bar{\mathbf{A}} \cdot (\bar{\mathbf{B}} \times \bar{\mathbf{C}}) = \bar{\mathbf{B}} \cdot (\bar{\mathbf{C}} \times \bar{\mathbf{A}}) = \bar{\mathbf{C}} \cdot (\bar{\mathbf{A}} \times \bar{\mathbf{B}})$	$\bar{\mathbf{A}} \times (\bar{\mathbf{B}} \times \bar{\mathbf{C}})$ <p>Lagrange's formula</p> $\bar{\mathbf{A}} \times (\bar{\mathbf{B}} \times \bar{\mathbf{C}}) = \bar{\mathbf{B}}(\bar{\mathbf{A}} \cdot \bar{\mathbf{C}}) - \bar{\mathbf{C}}(\bar{\mathbf{A}} \cdot \bar{\mathbf{B}})$ <p>Jacobi identity</p> $\bar{\mathbf{A}} \times (\bar{\mathbf{B}} \times \bar{\mathbf{C}}) + \bar{\mathbf{B}} \times (\bar{\mathbf{C}} \times \bar{\mathbf{A}}) + \bar{\mathbf{C}} \times (\bar{\mathbf{A}} \times \bar{\mathbf{B}}) = 0$ $(\bar{\mathbf{A}} \times \bar{\mathbf{B}}) \times \bar{\mathbf{C}} = \bar{\mathbf{A}} \times (\bar{\mathbf{B}} \times \bar{\mathbf{C}}) - \bar{\mathbf{B}} \times (\bar{\mathbf{A}} \times \bar{\mathbf{C}})$

Gradient theorem	$\int_a^b \nabla T \cdot d\vec{l} = T(b) - T(a)$
Divergence theorem ( Green , Gauss)	$\int_{\text{volume}} (\nabla \cdot \vec{V}) dv = \oint_{\text{surface}} \vec{V} \cdot d\vec{s}$
Curl Theorem ( Stoke)	$\int_{\text{surface}} (\nabla \times \vec{V}) \cdot d\vec{s} = \oint_{\text{line}} \vec{V} \cdot d\vec{l}$

Differential Element		
Cartesian	Cylindrical	Spherical
$dl = dx\vec{a}_x + dy\vec{a}_y + dz\vec{a}_z$  $d\vec{A}_x = dydz\vec{a}_x$ $d\vec{A}_y = dzdx\vec{a}_y$ $d\vec{A}_z = dxdy\vec{a}_z$  $dV = dxdydz$	$dl = d\rho\vec{a}_\rho + \rho d\phi\vec{a}_\phi + dz\vec{a}_z$  $d\vec{S}_x = \rho d\phi dz\vec{a}_\rho$ $d\vec{S}_y = dzd\rho\vec{a}_\phi$ $d\vec{S}_z = \rho d\rho d\phi\vec{a}_z$  $dV = \rho d\rho d\phi dz$	$dl = dr\vec{a}_r + r d\theta\vec{a}_\theta + r \sin\theta d\phi\vec{a}_\phi$  $d\vec{S}_r = r^2 \sin\theta \cdot d\theta d\phi\vec{a}_r$ $d\vec{S}_\theta = r \sin\theta \cdot dr d\theta\vec{a}_\theta$ $d\vec{S}_\phi = r dr d\theta\vec{a}_\phi$  $dV = r^2 \sin\theta dr d\theta d\phi$
Gradience ( scalar ) :		

$$\nabla f = \left( \frac{\partial f}{\partial x} \vec{a}_x + \frac{\partial f}{\partial y} \vec{a}_y + \frac{\partial f}{\partial z} \vec{a}_z \right)$$

### Div Laws (Vector)

$$\text{div } \mathbf{D} = \left( \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \right) \quad (\text{rectangular})$$

### Curl

$$\nabla \times \mathbf{A} = \begin{bmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x_A & y_A & z_A \end{bmatrix}$$

# GRADIENT

**RECTANGULAR**  $\nabla V = \frac{\partial V}{\partial x} \mathbf{a}_x + \frac{\partial V}{\partial y} \mathbf{a}_y + \frac{\partial V}{\partial z} \mathbf{a}_z$

**CYLINDRICAL**  $\nabla V = \frac{\partial V}{\partial \rho} \mathbf{a}_\rho + \frac{1}{\rho} \frac{\partial V}{\partial \phi} \mathbf{a}_\phi + \frac{\partial V}{\partial z} \mathbf{a}_z$

**SPHERICAL**  $\nabla V = \frac{\partial V}{\partial r} \mathbf{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \mathbf{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \mathbf{a}_\phi$

# DIVERGENCE

**RECTANGULAR**  $\nabla \cdot \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$

**CYLINDRICAL**  $\nabla \cdot \mathbf{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z}$

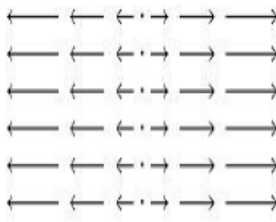
**SPHERICAL**  $\nabla \cdot \mathbf{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (D_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi}$

# CURL

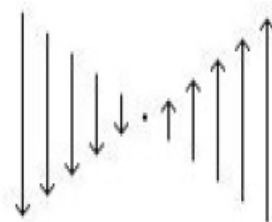
**RECTANGULAR**  $\nabla \times \mathbf{H} = \left( \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} \right) \mathbf{a}_x + \left( \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right) \mathbf{a}_y + \left( \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \mathbf{a}_z$

**CYLINDRICAL**  $\nabla \times \mathbf{H} = \left( \frac{1}{\rho} \frac{\partial H_z}{\partial \phi} - \frac{\partial H_\phi}{\partial z} \right) \mathbf{a}_\rho + \left( \frac{\partial H_\rho}{\partial z} - \frac{\partial H_z}{\partial \rho} \right) \mathbf{a}_\phi$   
 $+ \frac{1}{\rho} \left[ \frac{\partial (\rho H_\phi)}{\partial \rho} - \frac{\partial H_\rho}{\partial \phi} \right] \mathbf{a}_z$

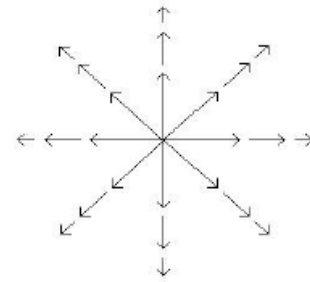
**SPHERICAL**  $\nabla \times \mathbf{H} = \frac{1}{r \sin \theta} \left[ \frac{\partial (H_\phi \sin \theta)}{\partial \theta} - \frac{\partial H_\theta}{\partial \phi} \right] \mathbf{a}_r + \frac{1}{r} \left[ \frac{1}{\sin \theta} \frac{\partial H_r}{\partial \phi} - \frac{\partial (r H_\phi)}{\partial r} \right] \mathbf{a}_\theta$   
 $+ \frac{1}{r} \left[ \frac{\partial (r H_\theta)}{\partial r} - \frac{\partial H_r}{\partial \theta} \right] \mathbf{a}_\phi$



Case 1: A vector field with positive divergence but zero curl.



Case 2: A vector field with nonzero curl (the curl vector points out of the computer screen), but zero divergence.



Case 3: An inverse square field. Its divergence has a value and curl is zero.

	Case 1	Case 2	Case 3
<b>Divergence</b>	$\nabla \cdot \vec{E} \neq 0$	$\nabla \cdot \vec{E} = 0$	$\nabla \cdot \vec{E} \neq 0$
<b>Curl</b>	$\nabla \times \vec{E} = 0$	$\nabla \times \vec{E} \neq 0$	$\nabla \times \vec{E} = 0$

خلاصة القول اللي تفهم بيه طريقه ال Div وال Curl تخيل الأسهم هي حركة موجات ميه والنقطه اللي بتدرس عندها فيها كورة بينج ، لو الكورة هتتحرك أي حته فوق تحت يمين شمال يبقى في Div موجود ، لو هتلف حوالين نفسها يبقى في curl لو هتتحرك وتلف حوالين نفسها الاتنين يبقى في الاتنين لو الموجات بتلاشي بعض وهتفضل ثابتة ومش هتتحرك يبقى مفيش حاجه

Symbol	Name	Unit	Abbreviation
$v$	Velocity	meter/second	m/s
$F$	Force	newton	N
$Q$	Charge	coulomb	C
$r, R$	Distance	meter	m
$\epsilon_0, \epsilon$	Permittivity	farad/meter	F/m
$E$	Electric field intensity	volt/meter	V/m
$\rho_v$	Volume charge density	coulomb/meter <sup>3</sup>	C/m <sup>3</sup>
$v$	Volume	meter <sup>3</sup>	m <sup>3</sup>
$\rho_L$	Linear charge density	coulomb/meter	C/m
$\rho_S$	Surface charge density	coulomb/meter <sup>2</sup>	C/m <sup>2</sup>
$\Psi$	Electric flux	coulomb	C
$D$	Electric flux density	coulomb/meter <sup>2</sup>	C/m <sup>2</sup>
$S$	Area	meter <sup>2</sup>	m <sup>2</sup>
$W$	Work, energy	joule	J
$L$	Length	meter	m
$V$	Potential	volt	V
$p$	Dipole moment	coulomb-meter	C·m
$I$	Current	ampere	A
$J$	Current density	ampere/meter <sup>2</sup>	A/m <sup>2</sup>
$\mu_e, \mu_h$	Mobility	meter <sup>2</sup> /volt-second	m <sup>2</sup> /V·s
$e$	Electronic charge	coulomb	C
$\sigma$	Conductivity	siemens/meter	S/m
$R$	Resistance	ohm	$\Omega$
$P$	Polarization	coulomb/meter <sup>2</sup>	C/m <sup>2</sup>
$\chi_{e,m}$	Susceptibility		
$C$	Capacitance	farad	F
$R_s$	Sheet resistance	ohm per square	$\Omega$
$H$	Magnetic field intensity	ampere/meter	A/m
$K$	Surface current density	ampere/meter	A/m
$B$	Magnetic flux density	tesla (or weber/meter <sup>2</sup> )	T (or Wb/m <sup>2</sup> )
$\mu_0, \mu$	Permeability	henry/meter	H/m
$\Phi$	Magnetic flux	weber	Wb
$V_m$	Magnetic scalar potential	ampere	A
$A$	Vector magnetic potential	weber/meter	Wb/m
$T$	Torque	newton-meter	N·m
$m$	Magnetic moment	ampere-meter <sup>2</sup>	A·m <sup>2</sup>
$M$	Magnetization	ampere/meter	A/m
$\mathcal{R}$	Reluctance	ampere-turn/weber	A·t/Wb
$L$	Inductance	henry	H
$M$	Mutual inductance	henry	H

Symbol	Name	Unit	Abbreviation
$\omega$	Radian frequency	radian/second	rad/s
$c$	Velocity of light	meter/second	m/s
$\lambda$	Wavelength	meter	m
$\eta$	Intrinsic impedance	ohm	$\Omega$
$k$	Wave number	meter <sup>-1</sup>	m <sup>-1</sup>
$\alpha$	Attenuation constant	neper/meter	Np/m
$\beta$	Phase constant	radian/meter	rad/m
$f$	Frequency	hertz	Hz
$S$	Poynting vector	watt/meter <sup>2</sup>	W/m <sup>2</sup>
$P$	Power	watt	W
$\delta$	Skin depth	meter	m
$\Gamma$	Reflection coefficient		
$s$	Standing wave ratio		
$\gamma$	Propagation constant	meter <sup>-1</sup>	m <sup>-1</sup>
$G$	Conductance	siemen	S
$Z$	Impedance	ohm	$\Omega$
$Y$	Admittance	siemen	S
$Q$	Quality factor		

## ELECTRIC FIELDS

Columbs Law :

$$\vec{F} = \frac{(Q_1 Q_2)}{4\pi\epsilon_0 R^2} \vec{a}_R = \frac{(Q_1 Q_2)}{4\pi\epsilon_0 R^3} \vec{R}$$

ElectricField Laws

Point Charge	Line charge	Infinitt line	
$E = \frac{Q}{4\pi\epsilon_0 R^3} \vec{R}$	$E = \int \frac{\rho_L dL}{4\pi\epsilon_0 R^2} \vec{a}_R$	$\vec{E} = \frac{\rho_L}{2\pi\epsilon_0 R} \vec{a}_R$	
Ring	Disk	Surface	Infinite surface
$E = \frac{\rho_0 a h}{2\epsilon_0 (a^2 + h^2)^{\frac{3}{2}}} \hat{a}_z$	$E = \frac{\rho_s}{2\epsilon_0} \left[ 1 - \frac{h}{\sqrt{h^2 + R^2}} \right]$	$E = \int \frac{\rho_s ds}{4\pi\epsilon_0 R^2} \vec{a}_R$	$E = \frac{\rho_s}{2\epsilon_0}$

Electric Flux – Flux density –gauss law

$$\psi = Q_{enc} = \oiint \vec{D} \cdot d\vec{s}$$

علاقه D بال E

$$D = \epsilon E \Rightarrow \frac{D}{E} = \epsilon \quad \therefore \quad D = \frac{E}{\epsilon}$$

Electric Density (D) relations

Point Charge	Infinitt line	Infinite surface	Cylindrical volume
$D = \frac{Q}{4\pi R^3} \vec{R}$	$\vec{D} = \frac{\rho_L}{2\pi R} \vec{a}_R$	$D = \frac{\rho_s}{2}$	$\rho < a$ $D = \frac{\rho_v}{2} \rho$ $\rho > a$ $\frac{\rho_v \left( \frac{a^2}{2} \right)}{\rho}$
Finite cylindrical surface	Finite spherical shell surface	Surface	
$D = \frac{\rho_s}{\rho} a$	$D = \rho_s \frac{a^2}{r^2}$	$D = \int \frac{\rho_s ds}{4\pi R^2} \vec{a}_R$	

Dot form of charge density

From green's or gauss theorem

$$\int_{\text{volume}} (\nabla \cdot \vec{V}) dv = \oint_{\text{surface}} \vec{V} \cdot d\vec{s}$$

$$\therefore \oiint \vec{D} \cdot d\vec{s} = \int \nabla \cdot \vec{D} dv = \int \rho_v dv$$

$$\therefore \nabla \cdot \vec{D} = \rho_v \quad \text{Maxwell's 1st equation}$$



## Energy and potential

$$W = - \int_{initial}^{final} q \vec{E} \cdot d\vec{L}$$

$$Note : W_{AB} = -W_{BA} \quad ; \quad W_{ABCD A} = 0$$

$$V_{AB} = - \int_B^A \vec{E} \cdot d\vec{L}$$

$$\oint \vec{E} \cdot d\vec{L} = 0$$

$$\vec{\nabla} \times \vec{E} = 0$$

**Maxwell's 2<sup>nd</sup> equation ( assuming conservative system )**

$$\oint \vec{E} \cdot d\vec{L} = \vec{\nabla} \times \vec{E} \neq 0 \text{ ( non – conservative system )}$$

Potential difference Equations :

Point Charge	Absolute potential	Line charge /Finite	Infinite line	Ring
$V_{AB} = \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r_A} - \frac{1}{r_B} \right]$	$V_A = V_{A\infty} = \frac{Q}{4\pi\epsilon_0 r_A}$	$V = \int \frac{\rho_L dL}{4\pi\epsilon_0 r} = \frac{\rho_L}{2\pi\epsilon_0} \ln \frac{L + \sqrt{L^2 + a^2}}{a}$	$V_{AB} = \frac{\rho_L}{2\pi\epsilon_0} \ln \frac{\rho_B}{\rho_A}$	$V = \frac{\rho_L a}{2\epsilon_0 \sqrt{a^2 + h^2}}$

Equipotential surfaces : surfaces that has the same potential

$$\frac{\Delta V}{\Delta L} = \text{Potential gradient}$$

$$V = - \int \vec{E} \cdot d\vec{L}$$

$$\Delta V = -E \Delta L$$

كمعيار

$$\therefore E = - \frac{\Delta V}{\Delta L}$$

كمتجه

$$\vec{E} = -\vec{\nabla} V$$

To move a charge from infinity to a point in the free space with other charges affect that point with a field

$$W_E = \frac{1}{2} \sum_{m=1}^n Q_m V_m$$

$$W_E = \frac{1}{2} \int \bar{D} \cdot \bar{E} \, dV \quad (J)$$

$$W_E = \frac{1}{2} \bar{D} \cdot \bar{E} \quad \left( \frac{J}{m^3} \right)$$

### Electrostatic Fields in materials

يمكننا تقسيم الشحنات لشحنه سطحيه و حجميه ، في الموصل نتعامل على ان السلك اسطوانه يمر بها شحنه حجميه  
العوامل اللي بتكون التيار ( كثافه الشحنات ، مساحه المقطع ، طول ، الزمن (سرعه الموصلات) )

$$i = \frac{\rho_v \Delta S \Delta L}{\Delta t} \quad (\text{divide by area})$$

$$J = \rho_v v_d$$

لا تعتمد على نوع توصيليه ماده ، تعتمد على نوع التوصيل conduction , convention

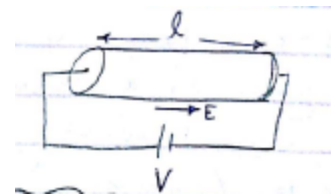
### Ohm's Law

$$J = \sigma \bar{E}$$

$$V = -\int E \cdot dL = E \cdot L$$

$$\text{ohm's law } J = \sigma E \Rightarrow \frac{I}{S} = \sigma \frac{V}{L} \Rightarrow \frac{V}{I} = \frac{L}{\sigma A} = R$$

$$\text{for non uniform } V : R = \frac{V}{I} = \frac{-\int E \cdot dL}{\int \sigma E \cdot dS}$$



### Field Effect on Dielectric Materials

يتم استقطاب ماده عند وجود مجال كهربي عليها

$$P = \chi_e \epsilon_0 \bar{E}$$

$$\chi_e = \epsilon_r - 1$$

اقل مجال كهربي يكسر العزم : Dielectric Strenght

$$D = \epsilon E = \epsilon_0 \epsilon_r E = \epsilon_0 (1 + \chi_e) E = P + \epsilon_0 E$$

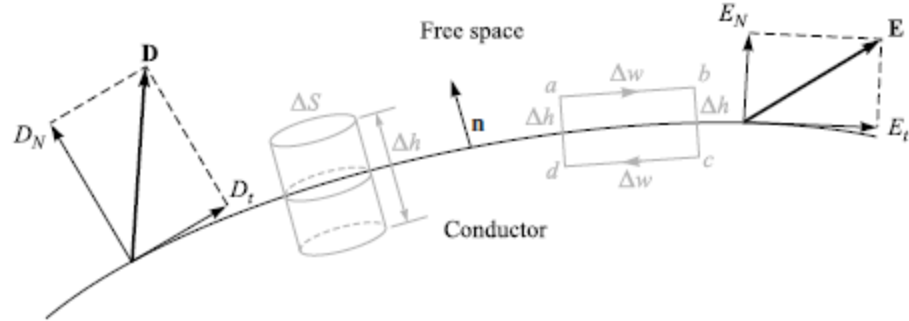
خواص المواد العازلة : (لا يوجد عزل مثالي

الماده العازلة لا تحتوي الكترونات حرة

عند التأثير على المواد العازلة يتم استقطابها

## Boundary Conditions

Between 1- Dielectric – Dielectric 2- Dielectric – Conductor



**Figure 5.4** An appropriate closed path and gaussian surface are used to determine boundary conditions at a boundary between a conductor and free space;  $E_t = 0$  and  $D_N = \rho_s$ .

1- Dielectric – Dielectric

Normal	Tangent
<p>Gauss (الشحنه على السطح الفاصل بين المادتين <math>\rho_s</math>)</p> $\oiint D \cdot dS = Q_{enc}$ $D_{1n} \Delta S - D_{2n} \Delta S = \rho_s \Delta S$ $D_{1n} - D_{2n} = \rho_s$ <p>if <math>\rho_s = 0</math></p> $\therefore D_{1n} = D_{2n}$	<p>Ampere's law</p> $\oint E \cdot dL = 0$ $\therefore E_{1t} \Delta w - E_{1n} \frac{\Delta h}{2} - E_{2n} \frac{\Delta h}{2} - E_{2t} \Delta w$ $+ E_{2n} \frac{\Delta h}{2} + E_{2n} \frac{\Delta h}{2} = 0$ $\therefore E_{1t} = E_{2t}$

2- Conductor – Dielectric

Normal	Tangent
<p>Gauss</p> $\oiint D \cdot dS = Q_{enc}$ $\therefore D_n = \rho_s$	$E_t = 0$

## Capacitance

$$C = \frac{Q}{V} \left( ( \text{if } E \text{ (electric field is uniform)} ) \right)$$

$$W_E = \frac{1}{2} C V^2 ; \text{Energy Density} = W = \frac{W_E}{AD} = \frac{1}{2} \epsilon_0 E^2$$

### ملحوظات للمكثفات

1- هيجي مساله مكثفات وش

2- المكثفات على التوالي

$$C_t = \frac{C_1 C_2}{C_1 + C_2}$$

المكثفات على التوازي

$$C_t = C_1 + C_2$$

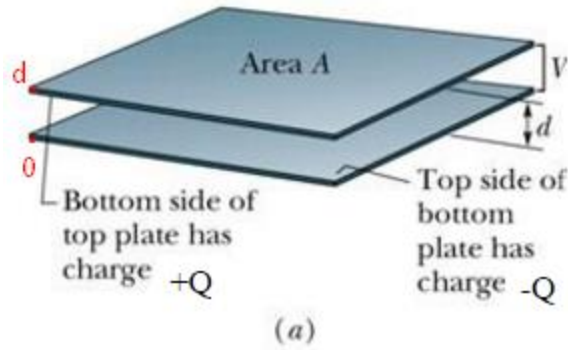
3- أنواع المكثفات ممكن يكون

Parallel plate- Coaxial ( cylindrical ) - Spherical

وركز في شكل المكثف والعدد في حاله اسطواني او كروي مش مستطيل

استنتاج قانون المكثف :

Parallel Plate :



$$C = \frac{Q}{V}$$

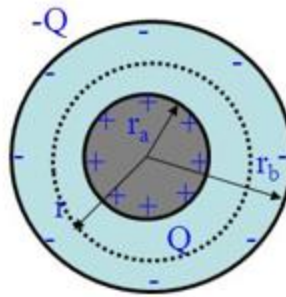
$$V = - \int_d^0 E \cdot dL$$

$$V = - \int_d^0 \frac{\rho_s}{\epsilon} \cdot dL$$

$$\therefore V = \frac{\rho_s}{\epsilon} d$$

$$\therefore C = \frac{Q}{V} = \frac{\rho_s A}{\frac{\rho_s d}{\epsilon}} = \frac{\epsilon A}{d}$$

## Spherical



$$\oint \vec{E} \cdot d\vec{A} = \frac{Q_{encl}}{\epsilon_0}$$

$$E(4\pi r^2) = \frac{Q}{\epsilon_0} \rightarrow E = \frac{Q}{4\pi\epsilon_0 r^2}$$

$$V = \frac{Q}{4\pi\epsilon_0 r}$$

$$V_{ab} = V_a - V_b = \frac{Q}{4\pi\epsilon_0 r_a} - \frac{Q}{4\pi\epsilon_0 r_b} = \frac{Q}{4\pi\epsilon_0} \frac{r_b - r_a}{r_a r_b}$$

$$C = \frac{Q}{V_{ab}} = 4\pi\epsilon_0 \frac{r_a r_b}{r_b - r_a}$$

## Cylindrical ( Co-axial )

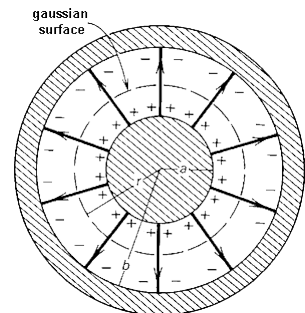
$$\oint \vec{E} \cdot d\vec{s} = \frac{Q_{enc}}{\epsilon_0} \Rightarrow E \cdot 2\pi r L = \frac{Q}{\epsilon_0}$$

$$E = \frac{Q}{2\pi\epsilon_0 r L}$$

$$V = \int_a^b E \cdot dr = \int_a^b \frac{Q}{2\pi\epsilon_0 r L} dr = \frac{Q}{2\pi\epsilon_0 L} \int_a^b \frac{1}{r} dr$$

$$V = \frac{Q}{2\pi L} \ln\left(\frac{b}{a}\right)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{2\pi L} \ln\left(\frac{b}{a}\right)} = \frac{2\pi\epsilon_0 L}{\ln\left(\frac{b}{a}\right)}$$



## MAGNETIC FIELDS

### The Sources of Magnetic Field :

1-Permanent magnet 2-Linearly changing electric field w/ time 3- a direct current

### Biot-Savart

$$H \propto \frac{m_1 m_2}{R^2} \quad \text{القوة المؤثرة على وحده الاقطاب المغناطيسية}$$

$$dH = \frac{Id\vec{L} \times \vec{a}_R}{4\pi R^2} = \frac{Id\vec{L} \times \vec{R}}{4\pi R^3}$$

The total current crossing any closed surface is zero. It is this current flowing in a closed circuit that must be our experimental source (In a closed path), not the differential element. It follows that only the integral form of the Biot-Savart law can be verified experimentally,  $\vec{H} = \oint \left( \frac{Id\vec{L} \times \vec{a}_R}{4\pi R^2} \right)$

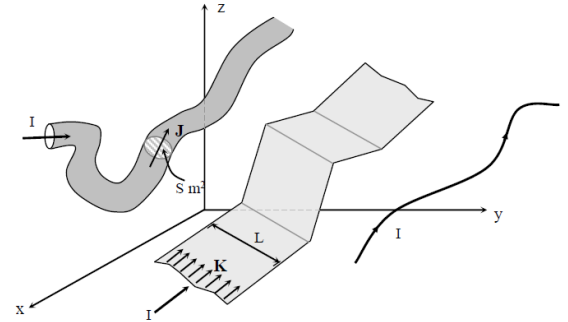
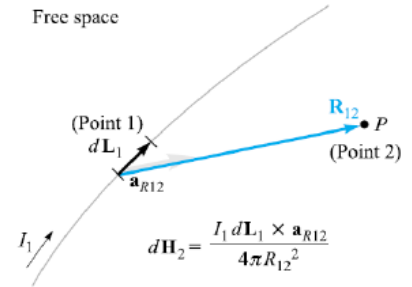
التيار الكهربائي هو اهم مصادر المجال المغناطيسي عشان كده لازم ندرس اشكاله المختلفه

Surface current density :  $I = K * L$  (uniform) or  $I = \int K dl$

the same with

$$Id\vec{L} = Kd\vec{s} = Jd\vec{V}$$

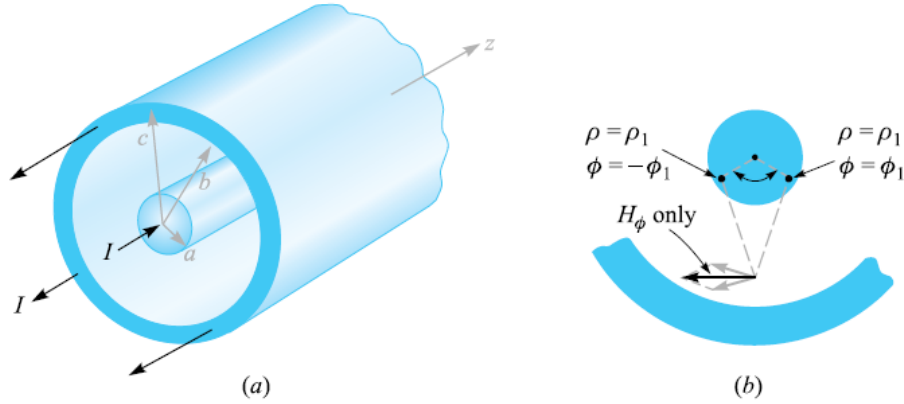
$$H = \int_s \frac{Kd\vec{s} \times \vec{a}_R}{4\pi R^2} = \int_v \frac{Jd\vec{v} \times \vec{a}_R}{4\pi R^2}$$



H from :

Infinite Line	Line
$H = \frac{I}{2\pi\rho} \vec{a}_\phi$	$H = \frac{I}{4\pi\rho} [\sin(\alpha_2) - \sin(\alpha_1)] \vec{a}_\phi$

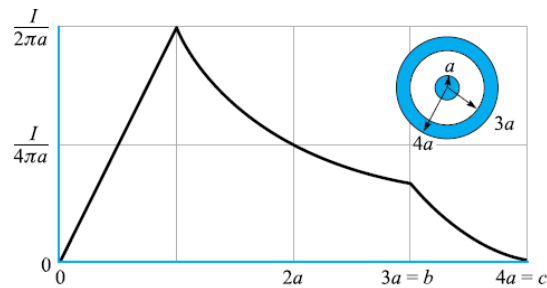
## H from Coaxial cable



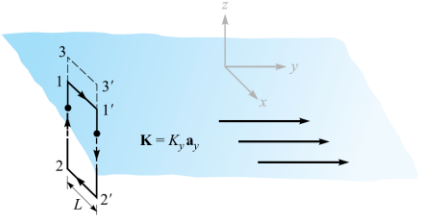
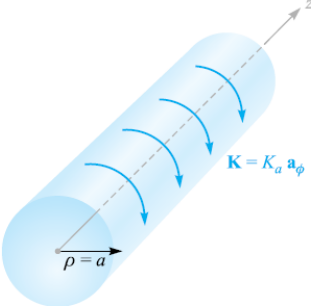
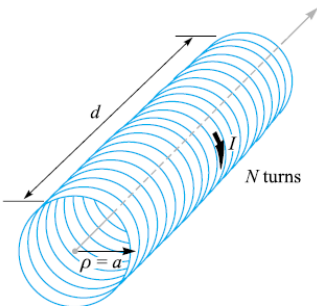
**Figure 7.8** (a) Cross section of a coaxial cable carrying a uniformly distributed current  $I$  in the inner conductor and  $-I$  in the outer conductor. The magnetic field at any point is most easily determined by applying Ampère's circuital law about a circular path. (b) Current filaments at  $\rho = \rho_1$ ,  $\phi = \pm\phi_1$ , produces  $H_\rho$  components which cancel. For the total field,  $H = H_\phi \mathbf{a}_\phi$ .

بتطبيق قانون امبير ( شبه قانون جاوس في الكهربائية )

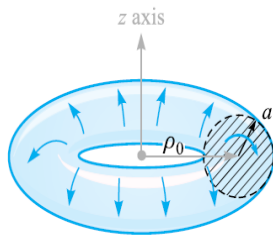
$\rho < a$	$a < \rho < b$	$b < \rho < c$	$\rho > c$
$I_{\text{encl}} = I \frac{\rho^2}{a^2}$ $2\pi\rho H_\phi = I \frac{\rho^2}{a^2}$ $H_\phi = \frac{I\rho}{2\pi a^2} \quad (\rho < a)$	$H_\phi 2\pi\rho = I$ $H_\phi = \frac{I}{2\pi\rho}$	$2\pi\rho H_\phi = I - I \left( \frac{\rho^2 - b^2}{c^2 - b^2} \right)$ $H_\phi = \frac{I}{2\pi\rho} \frac{c^2 - \rho^2}{c^2 - b^2} \quad (b < \rho < c)$	$H_\phi = 0 \quad (\rho > c)$



**Figure 7.9** The magnetic field intensity as a function of radius in an infinitely long coaxial transmission line with the dimensions shown.

<p>لاي نقطه على احد الجانبين</p> <div data-bbox="516 344 735 436"> <math display="block">\mathbf{H} = \frac{1}{2} \mathbf{K} \times \mathbf{a}_N</math> </div> 	<p>H from a surface</p>
<div data-bbox="289 667 597 970">  <p> <math>\mathbf{H} = K_a \mathbf{a}_z, \rho &lt; a</math>  <math>\mathbf{H} = 0, \rho &gt; a</math> </p> <p>(a)</p> </div> <div data-bbox="623 667 938 970">  <p> <math>\mathbf{H} = \frac{NI}{d} \mathbf{a}_z</math>              (well inside coil)           </p> <p>(b)</p> </div> <p><b>Figure 7.11</b> (a) An ideal solenoid of infinite length with a circular current sheet <math>\mathbf{K} = K_a \mathbf{a}_\phi</math>. (b) An <math>N</math>-turn solenoid of finite length <math>d</math>.</p> <p>لو محدود</p> $H = \frac{nl}{2} [\cos \theta_2 - \cos \theta_1]$	<p>H from a solenoid</p>



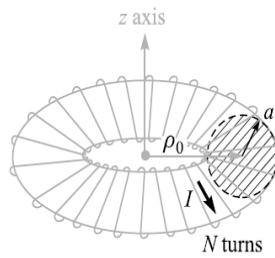


$$\mathbf{K} = K_a \mathbf{a}_z \text{ at } \rho = \rho_0 - a, z = 0$$

$$\mathbf{H} = K_a \frac{\rho_0 - a}{\rho} \mathbf{a}_\phi \text{ (inside toroid)}$$

$$\mathbf{H} = 0 \text{ (outside)}$$

(a)



$$\mathbf{H} = \frac{NI}{2\pi\rho} \mathbf{a}_\phi \text{ (well inside toroid)}$$

(b)

**Figure 7.12** (a) An ideal toroid carrying a surface current  $K$  in the direction shown. (b) An  $N$ -turn toroid carrying a filamentary current  $I$ .

H from a troid

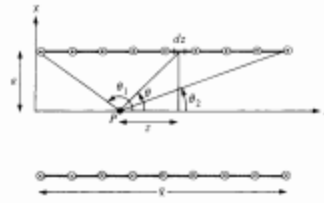


Figure 7.9 For Example 7.4; cross section of a solenoid.

**Solution:**

Consider the cross section of the solenoid as shown in Figure 7.9. Since the solenoid consists of circular loops, we apply the result of Example 7.3. The contribution to the magnetic field  $H$  at  $P$  by an element of the solenoid of length  $dz$  is

$$dH_z = \frac{I dl a^2}{2[a^2 + z^2]^{3/2}} = \frac{Ia^2 n dz}{2[a^2 + z^2]^{3/2}}$$

where  $dl = n dz = (N/\ell) dz$ . From Figure 7.9,  $\tan \theta = az/z$ ; that is,

$$dz = -a \operatorname{cosec}^2 \theta d\theta = -\frac{[z^2 + a^2]^{3/2}}{a^2} \sin \theta d\theta$$

Hence,

$$dH_z = -\frac{nI}{2} \sin \theta d\theta$$

or

$$H_z = -\frac{nI}{2} \int_{\theta_1}^{\theta_2} \sin \theta d\theta$$

Thus

$$\mathbf{H} = \frac{nI}{2} (\cos \theta_2 - \cos \theta_1) \mathbf{a}_z$$

as required. Substituting  $n = N/\ell$  gives

$$\mathbf{H} = \frac{NI}{2\ell} (\cos \theta_2 - \cos \theta_1) \mathbf{a}_z$$

At the center of the solenoid,

$$\cos \theta_2 = \frac{\ell/2}{[a^2 + \ell^2/4]^{1/2}} = -\cos \theta_1$$

and

$$\mathbf{H} = \frac{In\ell}{2[a^2 + \ell^2/4]^{1/2}} \mathbf{a}_z$$

If  $\ell \gg a$  or  $\theta_2 = 0^\circ$ ,  $\theta_1 = 180^\circ$ ,

$$\mathbf{H} = nI\mathbf{a}_z = \frac{NI}{\ell} \mathbf{a}_z$$

## Force from a Magnetic Field and Electric Field

As shown from the direction of  $H$  the Force from a magnetic field is in Right عموديه angle with the velocity of the particle

**Which means :** Magnetic Force can never change the velocity of a moving particle ; this means that magnetic field is incapable of transferring Energy to the moving charge

$$F_e(\text{Electric Force}) = Q\vec{E}$$

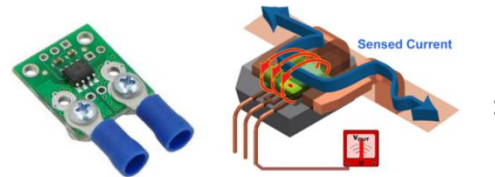
$$F_m(\text{Magnetic Force}) = Q \vec{V} \times \vec{B}$$

$$F_{total}(\text{Superposition force}) = Q(\vec{E} + \vec{V} \times \vec{B})$$

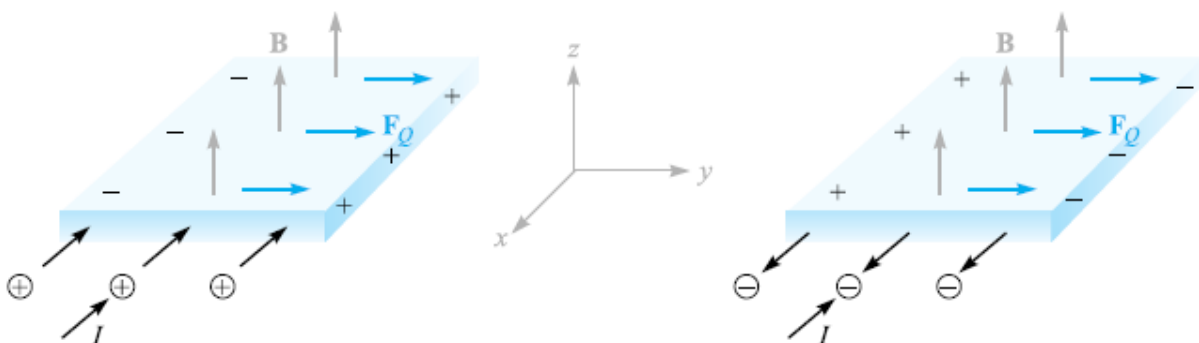
Notes : a large number of very small forces  $dF = dQ \vec{V} \times \vec{B}$  can cause electrons to shift slightly and then the conductor as a whole , it causes displacement in center of gravity between +ve and -ve charges so the columb (electric ) force tend to resist this displacement>

### What's Current sensor ( Hall Voltage )

It's a method to differentiate between the electrons and holes current by comparing their hall voltage in whats called current sensor this helps to determine if the semiconductor is n-type or p-type



The charge separation that does result, however, is disclosed by the presence of a slight potential difference across the conductor sample in a direction perpendicular to both the magnetic field and the velocity of the charges. The voltage is known as the Hall voltage, and the effect itself is called the Hall effect.



### Force on a current-carrying conductor

$$J = \rho_v \bar{v} \text{ and } Q = \rho_v dV$$

$$dF = dQ \bar{v} \times \bar{B} = \rho_v dV \frac{J}{\rho_v} \times \bar{B} = J dV \times \bar{B} = (J \times \bar{B}) dV$$

$$\text{the same } dF = (J \times \bar{B}) dV = (K \times \bar{B}) dS = (I \times \bar{B}) dL = IdL \times \bar{B}$$

$$\bar{F} = \int_v (J \times \bar{B}) dV = \int_s (K \times \bar{B}) dS$$

$$\bar{F} = \oint IdL \times \bar{B} = -I \oint \bar{B} \times dL = I \bar{L} \times \bar{B}$$

$$|F| = BIL \sin(\theta)$$

We can express Force between 2 current elements without the magnetic field but it will be complex as follows:

$$\text{from: } dF = I_2 d\bar{L}_2 \times \bar{B} \text{ \& } d\bar{H} = \frac{I_1 dL_1 \times a_R}{4\pi R^2} \text{ \& } B = \mu_0 H$$

$$\therefore F_2 = \mu_0 \frac{I_1 I_2}{4\pi} \oint [dL_2 \times \oint \frac{dL_1 \times a_R}{R^2}] \rightarrow (\text{very very complex})$$

**NOTE :** the total force on a closed current loop in a uniform = 0

## TORQUE

$$\vec{T} = \vec{R} \times \vec{F}$$

For a closed loop

$$d\vec{T} = I d\vec{S} \times \vec{B}$$

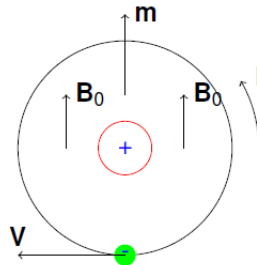
$$\text{define } d\vec{m} = I d\vec{S}$$

$$\therefore d\vec{T} = d\vec{m} \times \vec{B} \quad (\text{dipole moment } A.m^2)$$

$$\vec{T} = \vec{m} \times \vec{B} = I \vec{S} \times \vec{B}$$

The torque direction is that to align the magnetic field produced by the loop with the applied magnetic field causing the torque

في محاوله هنعتبر الالكترتون حوالين النواه يمثل لوب تياره عكس اتجاه حركه الالكترتون وتم تسليط فيض مغناطيسي خارجي ده هيسبب ان التيار بتاع حركه الالكترونات الصغير ده هيولد مجال مغناطيسي يحاول يحرك النواه في اتجاه المجال الخارجي لحد ما يبقوا aligned ويساعدو بعض - او يضادوا ! - على حسب



لهذا السبب

- 1- المجال المغناطيسي داخل المادة هيكون اكبر منه خارج المادة بسبب ان الالكترونات هتولد مجال إضافي داخلها
- 2- ال spin magnetic moment بتاع الالكترتون بتساوي  $9 \times 10^{-24} Am^2$  موجب لو بتساعد سالب لو بتضاد المجال الخارجي
- 3- الالكترونات اللي بتساهم بمجال مغناطيسي فقط الالكترونات اللي في المدارات الخارجيه غير المكتمله
- 4- طبعا كل الكلام اللي فوق ده محتاج معادلات من ميكانيكا الكم و حورات المهم اللي نستنتج ان نوع المادة وعدد الالكترونات و اللي بنكلم فيه ده جزء صغير جدا لان المادة مليانه moments لاسباب مختلفه وكلها بتاثر على تصنيف المادة المغناطيسيه الا ان التبسيط اللي فوق ده هو الأساس العلمي لاجهزه ال MRI ربنا لا يدخلكم في واحده

## Types Of Material

يمكن تصنيف المواد على حسب اذا كانت المومنت المحصله لالكترونات بتزود الفيض داخلها ام تقلله ام ماذا

**Table 8.1** Characteristics of magnetic materials

Classification	Magnetic Moments	B Values	Comments
Diamagnetic	$\mathbf{m}_{\text{orb}} + \mathbf{m}_{\text{spin}} = 0$	$B_{\text{int}} < B_{\text{appl}}$	$B_{\text{int}} \doteq B_{\text{appl}}$
Paramagnetic	$\mathbf{m}_{\text{orb}} + \mathbf{m}_{\text{spin}} = \text{small}$	$B_{\text{int}} > B_{\text{appl}}$	$B_{\text{int}} \doteq B_{\text{appl}}$
Ferromagnetic	$ \mathbf{m}_{\text{spin}}  \gg  \mathbf{m}_{\text{orb}} $	$B_{\text{int}} \gg B_{\text{appl}}$	Domains
Antiferromagnetic	$ \mathbf{m}_{\text{spin}}  \gg  \mathbf{m}_{\text{orb}} $	$B_{\text{int}} \doteq B_{\text{appl}}$	Adjacent moments oppose
Ferrimagnetic	$ \mathbf{m}_{\text{spin}}  \gg  \mathbf{m}_{\text{orb}} $	$B_{\text{int}} > B_{\text{appl}}$	Unequal adjacent moments oppose; low $\sigma$
Superparamagnetic	$ \mathbf{m}_{\text{spin}}  \gg  \mathbf{m}_{\text{orb}} $	$B_{\text{int}} > B_{\text{appl}}$	Nonmagnetic matrix; recording tapes

انن يمكننا تعريف 3 تيارات

1-  $I$  وهو التيار الذي نعرفه ناتج عن حركه الكترونات حره في موصل وفي قانون امبير  $\oint H \cdot dL = I$

2- التيار الناتج عن ال Bound charge والذي يعرف  $I_B$  وناتج عن المغناطيسية  $\oint M \cdot dL = I_B$

3- التيار الكلي وهو مجموع  $I_T = I_B + I$  ومن قانون امبير  $\oint \left(\frac{B}{\mu_0}\right) \cdot dL = I_T$

منها نستنتج عده قوانين هامه

$$\frac{B}{\mu_0} = M + H \quad \therefore \quad B = \mu_0 (H + M)$$

$$\oint M \cdot dL = I_B = \int_S J_B ds \quad \therefore \quad \nabla \times \vec{M} = \vec{J}_B$$

$$\oint H \cdot dL = I = \int_S J ds \quad \therefore \quad \nabla \times \vec{H} = \vec{J}$$

$$\oint \left(\frac{B}{\mu_0}\right) \cdot dL = I_T = \int_S J_T ds \quad \therefore \quad \nabla \times \frac{\vec{B}}{\mu_0} = \vec{J}_T$$

$$\text{where } \vec{M} = \text{atoms}/m^3 * (\text{dipole moment /atom}) = \frac{B}{\mu_0} \left( \frac{\chi_m}{1 + \chi_m} \right)$$

For Linear isotropic material ( if  $\chi_m$  magnetic susceptibility )  $M = \chi_m H$   
 $\therefore B = \mu_0 ( H + \chi_m H ) = \mu_0 (1 + \chi_m) H = \mu_0 \mu_r H$  where  $\mu_r = (1 + \chi_m)$   
define  $\mu = \mu_r \mu_0$   
then  **$B = \mu H$**

Generally :

As,

$$\bar{\mathbf{B}} = \mu \bar{\mathbf{H}}$$

for homogeneous, linear, isotropic magnetic material that may be described in terms of a relative permeability  $\mu_r$

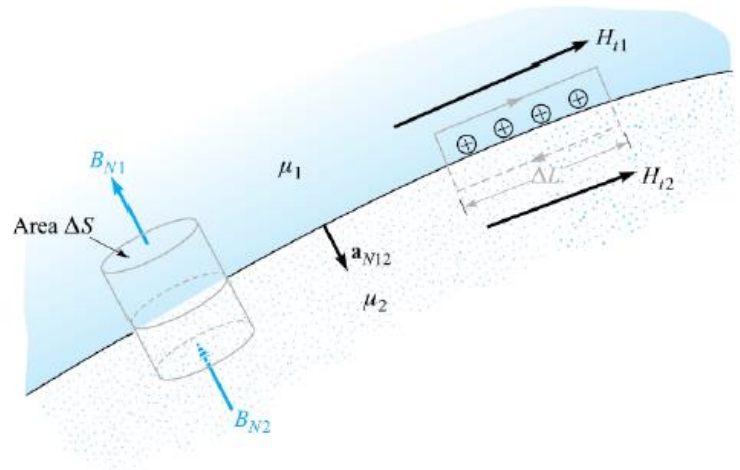
$$\begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \mu \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix}$$

For anisotropic materials

$$\begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \begin{bmatrix} \mu_{xx} & \mu_{xy} & \mu_{xz} \\ \mu_{yx} & \mu_{yy} & \mu_{yz} \\ \mu_{zx} & \mu_{zy} & \mu_{zz} \end{bmatrix} \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix}$$

الماتريكس المربعة اسمها tensor

## Boundary Conditions



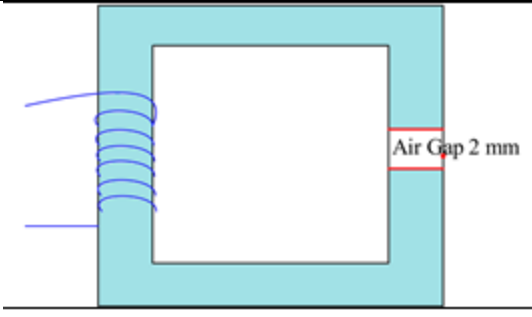
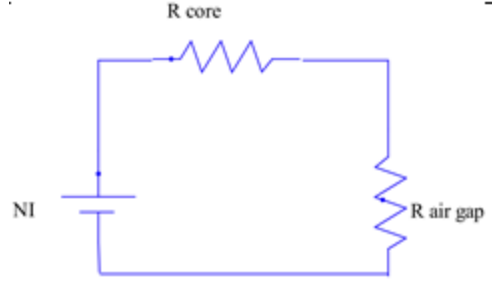
Normal	Tangent
$B_{N1} = B_{N2}$ $\mu_1 H_{N1} = \mu_2 H_{N2}$ $\frac{\mu_1 M_{N1}}{\chi_{m1}} = \frac{\mu_2 M_{N2}}{\chi_{m2}}$	$H_{t1} - H_{t2} = K$ $(H_{t1} - H_{t2}) \times a_{N12} = K$ $(H_{t1} - H_{t2}) = K \times a_{N12}$ $\frac{B_{t1}}{\mu_1} - \frac{B_{t2}}{\mu_2} = K$ $\frac{M_{t1}}{\chi_{m1}} - \frac{M_{t2}}{\chi_{m2}} = K$ <p>Where K (surface current) K = 0 if either materials is conductor</p>

## MAGNETIC CIRCUIT

طبعاً الجزئية دي احنا فاهمين تطبيقها من التحويل لكن الأساس الفيزيائي العلمي واضح من مقارنة المعادلات بين الكهربائية والمغناطيسية والتي ببساطة في تقريب الدائرة المغناطيسية لدائرة كهربائية ذات تيار مستمر ومقاومات فقط

MAGNETIC	ELECTRIC
1- $H = -\nabla V_m$	1- $E = -\nabla V$
2- $V_{mAB} = \int_A^B H \cdot dL$	2- $V_{AB} = \int_A^B E \cdot dL$
3- $B = \mu H$	3- $J = \sigma E$
4- $\phi = \int B \cdot ds$	4- $I = \int J \cdot dS$
5- $V_m = \phi \mathfrak{R}$	5- $V = IR$
6- $\mathfrak{R} = \frac{l}{\mu A}$	6- $R = \frac{l}{\sigma A}$
7- $\oint E \cdot dL = 0$	7- $\oint H \cdot dL = NI$
8- $W = \frac{1}{2} \int_v \vec{D} \cdot \vec{E} \, dv$	8- $W = \frac{1}{2} \int_v \vec{B} \cdot \vec{H} \, dv$
	$W = \frac{1}{2} \int_v \mu H^2 \, dv = \frac{1}{2} \int_v \frac{B^2}{\mu} \, dv$



Magnetic	Electrical
$Mmf = NI = \phi R = Hl$	$Emf = V = IR$
$R = \frac{l}{\mu A}$ $\mu = \mu_0 \mu_r$ $\mu_0 = 4\pi \times 10^{-7}$	$R = \frac{l}{\sigma A}$
	

## Inductance

**Flux Linkage ( $\lambda$ )** : the total flux linking the turns of a coil  $\lambda = N\phi$

المفروض عند حساب ال flux linkage نحسب فيض كل لفه الأول بس بدل ما نعمل كده بنستخدم ال winding factor and pitch factor لتصحيح الخطا في استخدام المعادله البسيطة

**Inductance ( $L$ ):** the ration between the flux linkage and the current it's linking

ويزيد الحث الذاتي كلما زاد عدد اللفات او الفيض وحدتها ال H .

## Inductance For a coaxial cable

$$a < \rho < b$$

$$H = \frac{I}{2\pi\rho} \Rightarrow B = \mu_0 H \Rightarrow \phi = \int_s B \cdot ds$$

$$\phi = \int_0^d \int_a^b \frac{\mu_0 I}{2\pi\rho} d\rho dz \quad a_\phi = \frac{\mu_0 I d}{2\pi} \ln \frac{b}{a}$$

$$L = \frac{N\phi}{I} = (\text{per meter lenght}) = \frac{\mu_0}{2\pi} \ln \frac{b}{a}$$

## Mutual Inductance

The mutual flux linking two coils

At  $90^\circ$  between coils it is  $M = 0$

At  $0^\circ$  between coils it is  $M_{\max}$

$$M_{12} = M_{21} = \frac{N_1 \phi_{12}}{I_2} = \frac{N_2 \phi_{21}}{I_1} \quad (H)$$

## Time Varying fields

As we know magnetic field varying with time can produce current

$$emf = -N \frac{d\phi}{dt}$$

( the -ve means that the flux act to produce an opposing flux (lenz' s law))

We can have  $\frac{d\phi}{dt}$  by

- 1- A time-varying flux with a stationary current path
- 2- A relative motion between the a steady flux and closed path
- 3- Combination of the two

## Kirchoff's Law

زمان أيام السيركتس والبراءة كنا بنقول ان كيرشوف بيقول ان محصله الجهود على مسار مغلق بتساوي صفر

$$\oint E \cdot dL = 0$$

لكن في حاله تولد emf مستحثه معدش  $= 0$  لان هيظهر عندي نوعين من الجهد

$$-1 \quad -\frac{d\phi}{dt} = -\frac{d}{dt} \int_s B \cdot ds \quad \text{ناتج عن تغير الفيض مع الزمن}$$

$$-2 \quad \frac{F}{Q} = E_m = v \times B \quad \text{ناتج عن الحركه}$$

لذا

$$emf = \oint E \cdot dL = \int_s -\frac{\partial B}{\partial t} ds = \oint (\bar{v} \times \bar{B}) dL$$

$$\text{transform voltage only } emf = \oint E \cdot dL = \int_s (\nabla \times E) ds = \int_s -\frac{\partial B}{\partial t} ds$$

$$\therefore \nabla \times E = -\frac{\partial B}{\partial t}$$

$$\text{Motional voltage only } emf = \oint E \cdot dL = \oint (\bar{v} \times \bar{B}) dL$$

## Displacement Current

زمان أيام السيركتس والبراءة كنا بنقول ان المكثف مبيمرش فيه تيار وكنا بنقول ان قانون امبير بسيط وبيقولك

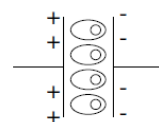
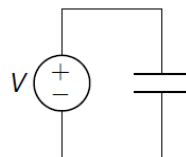
$$\oint H \cdot dl = I \quad \text{or} \quad \nabla \times H = J$$

لكن للتجارب العمليه في ال timed varying fields كان في جزء ناقص من المعادله دي وهو ال Displacement Current  $I_d$

$$\oint H \cdot dl = I + I_d = I + \int_s \frac{dD}{dt} \cdot ds \quad \text{or} \quad \nabla \times H = J + J_d = J + \frac{dD}{dt}$$

وممكن نستنتج المقدار ده  $\frac{dD}{dt}$  كالاتي

$$\begin{aligned} C &= \frac{\epsilon A}{d} ; V = \int E \cdot dL = Ed \\ \therefore I &= JA = C \frac{dv}{dt} = \frac{\epsilon A}{d} * d * \frac{dE}{dt} = \epsilon \frac{dE}{dt} * A = \frac{dD}{dt} * A \\ \therefore J_d &= \frac{dD}{dt} = \epsilon \frac{dE}{dt} \end{aligned}$$



## MAXWELL EQUATIONS

Differential Form	Integral Form
$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\oint \vec{E} \cdot d\vec{L} = -\int_s \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$
$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$	$\oint \vec{H} \cdot d\vec{L} = I + \int_s \frac{\partial \vec{D}}{\partial t} \cdot d\vec{S}$
$\nabla \cdot \vec{D} = \rho$	$\oint_s \vec{D} \cdot d\vec{s} = \int_v \rho_v \cdot dv$
$\nabla \cdot \vec{B} = 0$	$\oint_s \vec{B} \cdot d\vec{s} = 0$

Auxiliary Equations :

$$\begin{array}{lll} \vec{D} = \epsilon \vec{E} & \vec{D} = \epsilon_0 \vec{E} + \vec{P} & \vec{P} = \chi_e \epsilon_0 \vec{E} \\ \vec{B} = \mu \vec{H} & \vec{B} = \mu_0 (\vec{H} + \vec{M}) & \vec{M} = \chi_m \vec{H} \\ \vec{J} = \sigma \vec{E} & \vec{J} = \rho_v \vec{V} & \end{array}$$

And God said,  
" $\nabla \cdot \mathbf{D} = \rho$   
 $\nabla \cdot \mathbf{B} = 0$   
 $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$   
 $\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$ "  
and there was light.

1.27. The surfaces  $r = 2$  and  $4$ ,  $\theta = 30^\circ$  and  $50^\circ$ , and  $\phi = 20^\circ$  and  $60^\circ$  identify a closed surface.

a) Find the enclosed volume: This will be

$$\text{Vol} = \int_{20^\circ}^{60^\circ} \int_{30^\circ}^{50^\circ} \int_2^4 r^2 \sin \theta dr d\theta d\phi = \underline{2.91}$$

where degrees have been converted to radians.

b) Find the total area of the enclosing surface:

$$\begin{aligned} \text{Area} = \int_{20^\circ}^{60^\circ} \int_{30^\circ}^{50^\circ} (4^2 + 2^2) \sin \theta d\theta d\phi + \int_2^4 \int_{20^\circ}^{60^\circ} r(\sin 30^\circ + \sin 50^\circ) dr d\phi \\ + 2 \int_{30^\circ}^{50^\circ} \int_2^4 r dr d\theta = \underline{12.61} \end{aligned}$$

c) Find the total length of the twelve edges of the surface:

$$\begin{aligned} \text{Length} = 4 \int_2^4 dr + 2 \int_{30^\circ}^{50^\circ} (4 + 2) d\theta + \int_{20^\circ}^{60^\circ} (4 \sin 50^\circ + 4 \sin 30^\circ + 2 \sin 50^\circ + 2 \sin 30^\circ) d\phi \\ = \underline{17.49} \end{aligned}$$

1.27. (continued)

d) Find the length of the longest straight line that lies entirely within the surface: This will be from  $A(r = 2, \theta = 50^\circ, \phi = 20^\circ)$  to  $B(r = 4, \theta = 30^\circ, \phi = 60^\circ)$  or

$$A(x = 2 \sin 50^\circ \cos 20^\circ, y = 2 \sin 50^\circ \sin 20^\circ, z = 2 \cos 50^\circ)$$

to

$$B(x = 4 \sin 30^\circ \cos 60^\circ, y = 4 \sin 30^\circ \sin 60^\circ, z = 4 \cos 30^\circ)$$

or finally  $A(1.44, 0.52, 1.29)$  to  $B(1.00, 1.73, 3.46)$ . Thus  $\mathbf{B} - \mathbf{A} = (-0.44, 1.21, 2.18)$  and

$$\text{Length} = |\mathbf{B} - \mathbf{A}| = \underline{2.53}$$

سؤال : يعطى  $\vec{D}$  ويطلب  $\psi$  .

هناك طريقتين للحل :

$$\textcircled{1} \psi = Q_{enc} = \oint \vec{D} \cdot d\vec{s}$$

$$\textcircled{2} \psi = Q_{enc} = \int \rho_v dV, \rho_v = \nabla \cdot \vec{D}$$

لا يخلو امتحان من هذا السؤال

$$\text{Example : } \vec{D} = (4x, 3y^2, 2z^3)$$

$$1 \leq x \leq 2$$

$$2 \leq y \leq 3$$

$$3 \leq z \leq 4$$

Find  $\psi$  .

$\Delta y \Delta z$

$$\text{Sol : } \psi = 93 \text{ C}$$

$$\text{Example : } \vec{E} = -8xy \vec{a}_x - 4x^2 \vec{a}_y + 4z \vec{a}_z$$

$$Q = 6 \text{ C}$$

$$B(1, 8, 5) \rightarrow A(2, 18, 6)$$

Find  $W$

$$W = -Q \int_B^A \vec{E} \cdot d\vec{L}$$

طريقه الحل : نحاذي بعمل البركه على ٣ مراحل  
كل مرحله بنقل احداثي واحد ونثبت الثانيين  
على وضعهم السابقه للحركه على اياي

$$\rightarrow (2, 8, 5)$$

$$\rightarrow (2, 18, 5)$$

$$\rightarrow (2, 18, 6)$$

$$W = -Q \left[ \int_{z=5}^2 E_x dx + \int_{y=8}^{18} E_y dy + \int_{x=2}^6 E_z dz \right]$$

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